# Recent advances in high-order mesh adaptivity using the target-matrix optimization paradigm

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- Introduction
- Overview of Target Matrix Optimization Paradigm (TMOP) for r-adaptivity
- Recent advances
  - Target construction and mesh quality metrics
  - *hr*-adaptivity
  - Tangential relaxation and interface fitting
- Future work







### Introduction

Why mesh optimization?



Outwards propagating shock wave



Multimaterial Lagrangian hydrodynamics

- Mesh optimization can help adapt the mesh to the solution and ultimately reduce error.
- Improve conditioning of the resulting system.







# **Target Matrix Optimization Paradigm (TMOP)**



 Any Jacobian transformation can be represented using four geometric parameters:

$$W = \underbrace{\zeta} \quad \underbrace{R} \quad \underbrace{Q} \quad \underbrace{D}$$
[volume] [rotation] [skewness] [aspect-ratio]

 The transformation T from the active to target element can be defined using the Jacobian transformation A and W.





#### **TMOP Mesh Quality Metrics**

- Quality metric  $\mu(T)$  is a measure of the deviation between the active and target Jacobian transformation.
- Different metrics depend on different geometric parameters.
  - Shape metric depends on Skew (Q) and Aspect-ratio (D).  $\mu_2(T) = 0.5 \frac{|T|^2}{\det(T)} 1$

• Size metric - depends on 
$$\zeta$$
.  $\mu_{77}(T) = 0.5 \left( \det(T) - \frac{1}{\det(T)} \right)^2$ 

- Other kinds include Alignment, Shape + Size, Shape + Alignment, etc.
- We typically deploy Shape + Size metrics but seldom also use Alignment metrics.





#### **Node Movement with TMOP**

 Using the quality metric and the Jacobian transformation T, the TMOP objective function is defined as:

$$F(\mathbf{x}) = \sum_{E \in \mathcal{M}} F_E(\mathbf{x}_E) = \sum_{E(\mathbf{x}_E)} \int_{E_t} \omega(\mathbf{x}) \mu(T(\mathbf{x})) d\mathbf{x}_t$$

where x represents mesh coordinates,  $\omega$  is a user-defined spatial weight. The element-by-element integral is computed as:

$$\sum_{E \in \mathcal{M}} \int_{E_t} \omega(\mathbf{x}_t) \mu(T(\mathbf{x}_t)) d\mathbf{x}_t = \frac{1}{N_E} \sum_{E \in \mathcal{M}} \sum_{\mathbf{x}_q \in E_t} w_q \det(W(\bar{\mathbf{x}}_q)) \, \omega(\mathbf{x}_q) \mu(T(\mathbf{x}_q))$$

- In practice, we can use multiple metrics with different spatial weights.
- r-adaptivity  $F(\mathbf{x})$  is minimized using a technique such as the Newton's method to optimize the mesh [2].





#### **Target Construction & Mesh Quality Metric**

- Use of TMOP relies on choice of W and a compatible quality metric satisfying certain convexity requirements.
- Recent developments have advanced the state-of-the-art on both fronts.







#### **Target Construction**

Knupp describes various techniques with examples in "Target formulation and construction in mesh quality improvement", LLNL-TR-795097.







#### **Metric polyconvexity**

- Existence of minimum can be established, in part, by showing that the metric is polyconvex [Garanzha].
- Knupp has developed various metrics for TMOP in *"Metric type in the target-*matrix mesh optimization paradigm", LLNL-TR-817490.
  - Over 100 different metrics divided into 8 Types based on geometric properties.
  - Analyzes polyconvexity of each metric.
  - Determined at-least one polyconvex metric for Shape, Shape + Size, Orientation + Size, and Shape + Orientation + Size.







# **Simulation-driven Adaptivity**



Simulation data material indicator ( $\eta$ )







- $\phi = \frac{\pi}{2}$  for an ideal square.
- Use a Shape + Size polyconvex metric,  $\mu_{80} = (1 \gamma)\mu_2 + \gamma \mu_{77}$ .

$$\mu_2(T) = 0.5 \frac{|T|^2}{\det(T)} - 1 \qquad \mu_{77}(T) = \frac{1}{2} (\tau - \frac{1}{\tau})^2$$

• Note:  $\eta$  must be remapped between and after Newton iterations.

"Simulation-driven optimization of high-order meshes in ALE hydrodynamics." Computers & Fluids 208 (2020): 104602.







# hr-adaptivity

- Effectiveness of *r*-adaptivity can be limited due to the topology of the original mesh.
- *h*-adaptivity introduces addition degrees of freedom by splitting existing elements.
- Nonconforming high-order mesh refinement framework introduced by Cerveny et al. [6]
  - Supports nonconforming isotropic and anisotropic refinement/derefinement in 2D and 3D for triangles/quads and tetrahedrons/cubes.
  - Requires use of an error estimator for refinement/derefinement decisions during simulation.







### **AMR for Mesh Optimization**



Different types of refinements for a quad and a cube

- Anisotropic refinements impact the shape and size of an element, and isotropic refinement impacts only the size of an element.
- Refinements also impact skew, but this impact cannot be directly controlled.





#### **TMOP-based Refinement Error Estimator**

- Based on  $\mu$ , define  $\Gamma$  as the set of refinement types to be considered:
  - Shape metric  $\gamma = 1,2$  in 2D and 1-6 in 3D.
  - Size metric  $\gamma = 3$  in 2D and 7 in 3D.
  - Shape + Size metric  $\gamma = 1 3$  in 2D and 1-7 in 3D.
- For a given element *E* and refinement type  $\gamma \in \Gamma$ :

Difference in energy for a given refinement. Sum of TMOP energy for children of a given element. TMOP energy for a given element.  $F_E = \sum_{i=1}^{N_c} F_{E_c}$   $F_E = \sum_{\mathbf{x}_q \in E_t} w_q \det(W(\bar{\mathbf{x}}_q)) \omega(\mathbf{x}_q) \mu(T(\mathbf{x}_q))$ • Refinement type is picked based on:  $\max_{\gamma} \Delta F_E^{\gamma}, \gamma \in \Gamma$ 





#### **TMOP-based Derefinement Error Estimator**

- Derefinement is important for time-dependent problems where regions that require resolution can change with time.
- Elements that are already refined, are considered for derefinement:
  - If  $E_p$  is an element that was refined to span  $N_c$  children at a previous iteration:

ifference in energy for a 
$$\Delta F_{E_p} = \sum_{i=1}^{N_c} \frac{F_{E_c}}{N_c} - F_{E_p}$$

- $\Delta F_E^{\gamma}$  for refinement and  $\Delta F_{E_p}$  for derefinement are compliments of each other.
- Note: Determining  $\Delta F_E^{\gamma}$  and  $\Delta F_{E_p}$  requires the discrete functions to be mapped between children and parent elements.

D





# hr-adaptivity







#### **2D Benchmark Using Poisson Equation**

Solve the Poisson problem:

$$\nabla^2 u = f, \qquad \Omega = [0,1]^2$$

with a known exact solution to mimic a sharp circular wave front of radius r centered at  $(x_c, y_c)$ 

$$u = \arctan\left[\alpha \left(\sqrt{(x - x_c)^2 + (y - y_c)^2} - r\right)\right]$$

• 
$$\alpha = 200, (x_c, y_c) = (-0.05, -0.05), r = 0.7$$









#### **2D Benchmark Using Poisson Equation**

Target construction using gradient of the discrete function on the mesh, as earlier.

$$W = \sqrt{\zeta} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & \cos \phi \\ 0 & \sin \phi \end{bmatrix} \begin{bmatrix} \frac{1}{\sqrt{\rho}} & 0 \\ 0 & \sqrt{\rho} \end{bmatrix}$$

 To compare h-, r-, and hr-adaptivity, we start with a mesh and do 1 iteration of h- and/or r-adaptivity, using a Shape + Size metric





### **2D Benchmark Using Poisson Equation**

- Error comparison for different adaptivity techniques shows effectiveness of *hr*-adaptivity.









# **Application to ALE Hydrodynamics**

- Triple point problem using Laghos in MFEM.
- Large mesh deformations lead to mesh tangling in Lagrangian framework.
- TMOP-based r- and hr-adaptivity improves mesh quality and provides resolution in regions with material interaction.



"hr-Adaptivity for nonconforming high-order meshes with the target matrix optimization paradigm." Engineering with Computers (2021): 1-17.





- The surface of interest is given as a discrete level set (no analytic parametrization).
- Penalty formulation (quality / fitting tradeoff).
  - All mesh nodes move simultaneously.
  - One approach for fitting / tangential relaxation.

$$F(x) = F_{\mu} + w_{\sigma} \int_{\Omega} \bar{\sigma}(x)^2$$

- The restricted level set function \$\overline{\sigma}\$ penalizes the deviation from the zero level set.
  - Marking is not a trivial procedure.









We restrict σ to the set of marked nodes:

$$\bar{\sigma}_i = \begin{cases} \sigma_i & \text{if } i \in \mathcal{S}, \\ 0 & \text{otherwise.} \end{cases}$$

• Goal: move the mesh so that  $\sigma_i \equiv \sigma(\mathbf{x}_i) = 0$ . - Interpolatory finite element basis functions.



• Requires derivative computation,  $\frac{\partial \sigma}{\partial \mathbf{x}}$ , and transfer of  $\sigma(\mathbf{x}_0)$  as the mesh moves during optimization.

"Adaptive Surface Fitting and Tangential Relaxation for High-Order Mesh Optimization", International Meshing Roundtable, 2021.











• For non-smooth practical cases, further research and methods are required.









- Theoretical and practical advances in target construction and metric types for TMOP.
- TMOP-based *hr*-adaptivity for nonconforming high-order meshes helps improve mesh quality while reducing DOFs required for a given accuracy in solution.
  - Dobrev et al. "hr-adaptivity for nonconforming high-order meshes with the target matrix optimization paradigm". Engineering With Computers, 2021.
- Surface fitting and tangential relaxation through an adaptive FE formulation.
  - Discrete representation of the surface; no analytic parametrization
  - Weak enforcement through a variational penalty term
- All presented methods are (or will be) available in MFEM.



mfem.org



glvis.org









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